CH2407 Process Equipment Design II

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Heat Exchanger Design

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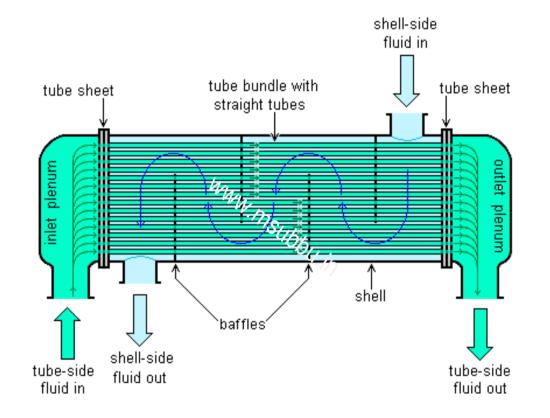
14-July-2011

Contents

- Single pass and multi-pass exchangers
- Heat transfer rate
- Temperature difference between two streams
- Heat transfer coefficient estimations
- Allocation of fluid in shell and tube exchangers
- Baffle spacing
- Pressure drop calculation
- Design codes

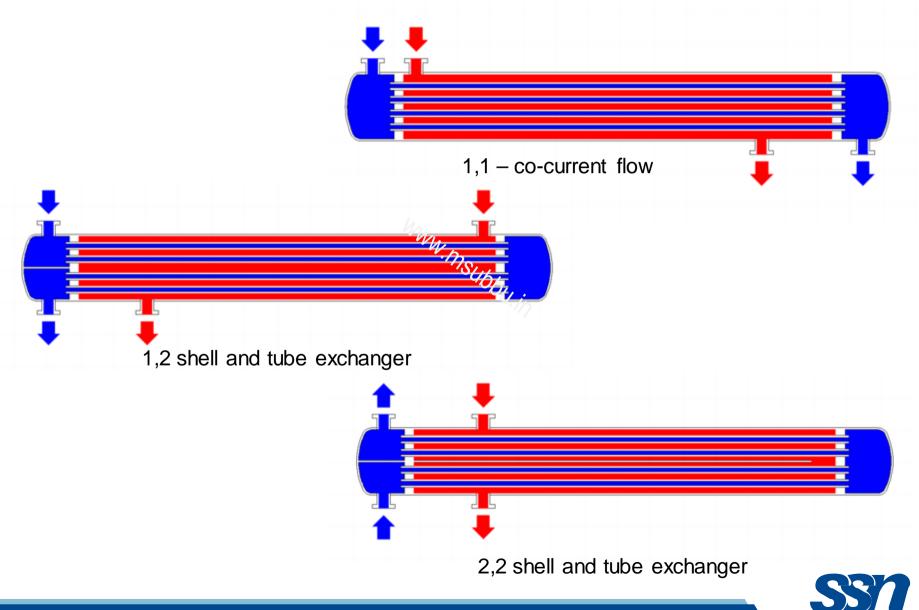


Shell and Tube Heat Exchanger





Pass Arrangements



Heat Transfer Rate

 $Q = UA\Delta T_m \longrightarrow 1$

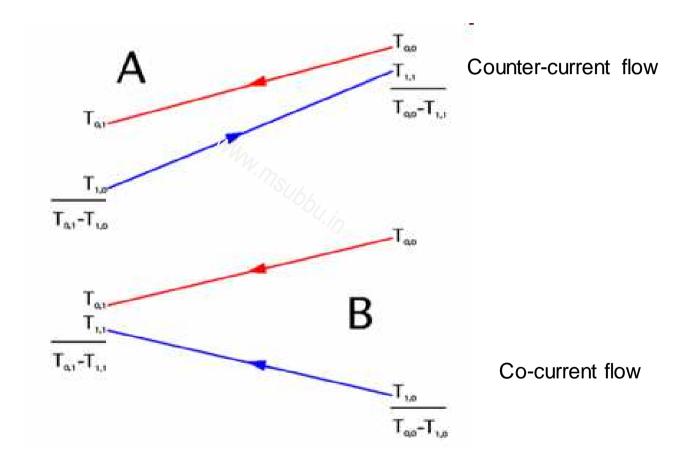
where Q = heat transferred per unit time, W, U = the overall heat transfer coefficient, $W/m^2 \circ C$, A = heat-transfer area, m^2 , ΔT_m = the mean temperature difference, the temperature driving force, $\circ C$.

From first law of thermodynamics,

$$Q = mC_p dT$$

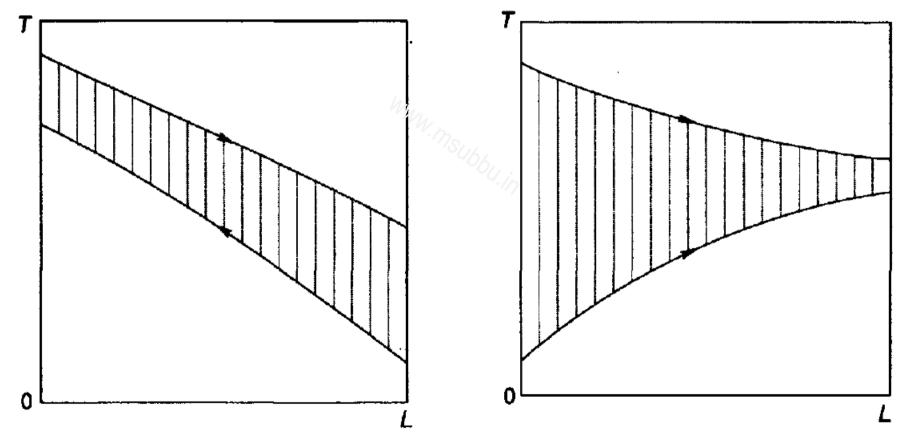


Temperature profile



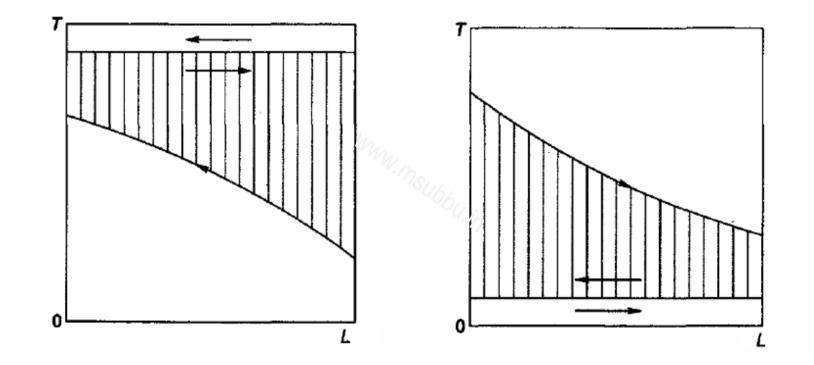


Co-current and counter-current flows



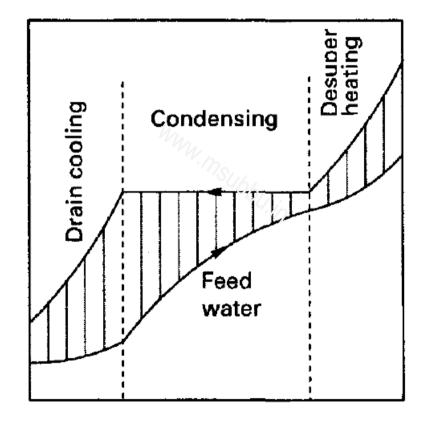


One fluid at constant temperature



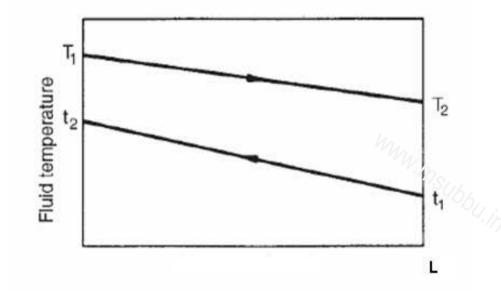


Temperature profile of condenser with de-superheating





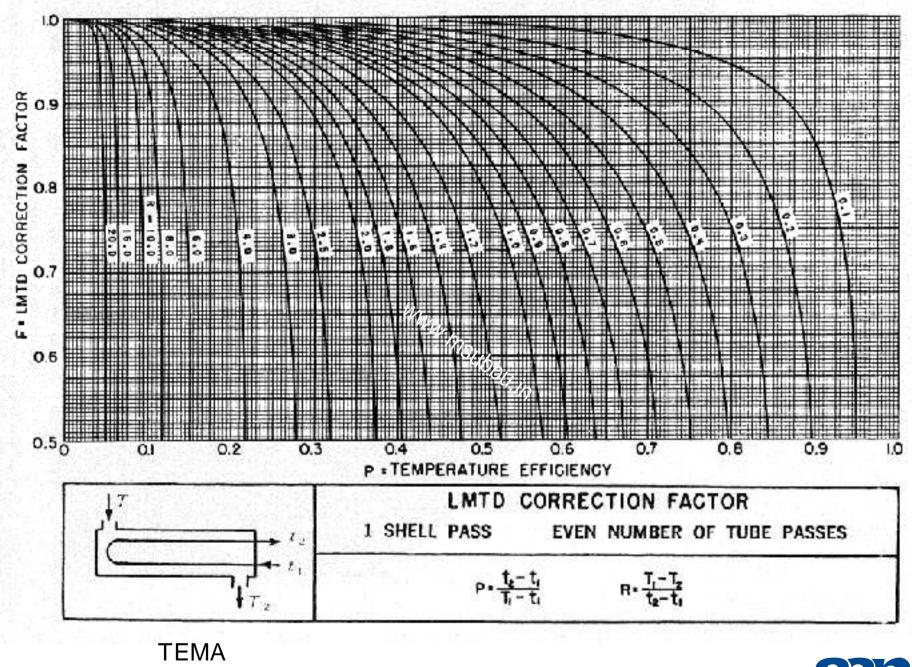
Temperature Difference



$$\Delta T_{\rm lm} = \frac{(T_1 - t_2) - (T_2 - t_1)}{\ln \frac{(T_1 - t_2)}{(T_2 - t_1)}}$$

$$\Delta T_m = F_t \Delta T_{\rm lm}$$









Overall Heat Transfer Coefficient

$$\frac{1}{U_o} = \frac{1}{h_o} + \frac{1}{h_{od}} + \frac{d_o \ln\left(\frac{d_o}{d_i}\right)}{2k_w} + \frac{d_o}{d_i} \times \frac{1}{h_{id}} + \frac{d_o}{d_i} \times \frac{1}{h_i}$$

where $U_o =$ the overall coefficient based on the outside area of the tube, W/m²°C,

- h_o = outside fluid film coefficient, W/m²°C,
- h_i = inside fluid film coefficient, W/m²°C,
- h_{od} = outside dirt coefficient (fouling factor), W/m²°C,
- h_{id} = inside dirt coefficient, W/m²°C,
- k_w = thermal conductivity of the tube wall material, W/m°C,
- d_i = tube inside diameter, m,
- d_o = tube outside diameter, m.



	Shell an	d tube exchangers	
	Hot fluid	Cold fluid	$U (W/m^2 °C)$
	Heat exchangers		
	Water	Water	800-1500
	Organic solvents	Organic solvents	100-300
	Light oils	Light oils	100 - 400
	Heavy oils	Heavy oils	50-300
	Gases	Gases	10 - 50
	Coolers		
	Organic solvents	Water	250-750
	Light oils	Water	350-900
	Heavy oils	Water	60-300
	Gases	Water	20-300
	Organic solvents	Brine	150-500
	Water	Brine	600-1200
	Gases	Eripe	15-250
	Heaters		
	Steam	Water	1500-4000
	Steam	Organic solvents	500-1000
	Steam	Light oils	300-900
	Steam	Heavy oils	60 450
	Steam	Gases	30-300
	Dowtherm	Heavy oils	50-300
	Dowtherm	Gases	20-200
	Flue gases	Steam	30-100
	Flue	Hydrocarbon vapours	30-100
	Condensers		
Coulson &	Aqueous vapours	Water	1000-1500
Richardson Vol.6	Organic vapours	Water	700-1000
	Organics (some non-condensables)	Water	500-700
ed.4	Vacuum condensers	Water	200-500
	Vaporisers		
	Steam	Aqueous solutions	1000 - 1500
	Steam	Light organics	900-1200
14-July-2011 M Sub	Steam	Heavy organics	600-900

Table 12.1. Typical overall coefficients



Fluid	$Coefficient~(W/m^{2}{}^{\circ}C)$	Factor (resistance) (m ²⁰ C/W)
River water	3000-12,000	0.0003 - 0.0001
Sea water	1000-3000	0.001 - 0.0003
Cooling water (towers)	3000-6000	0.0003 - 0.00017
Towns water (soft)	3000-5000	0.0003 - 0.0002
Towns water (hard)	1000-2000	0.001 - 0.0005
Steam condensate	1500-5000	0.00067 - 0.0002
Steam (oil free)	4000-10,000	0.0025 - 0.0001
Steam (oil traces)	2000 5000	0.0005 0.0002
Refrigerated brine	3000-5900	0.0003-0.0002
Air and industrial gases	5000-10,000	0.0002 - 0.0001
Flue gases	2000-5000	0.0005 - 0.0002
Organic vapours	5000	0.0002
Organic liquids	5000	0.0002
Light hydrocarbons	5000	0.0002
Heavy hydrocarbons	2000	0.0005
Boiling organics	2500	0.0004
Condensing organics	5000	0.0002
Heat transfer fluids	5000	0.0002
Aqueous salt solutions	3000-5000	0.0003 - 0.0002

Table 12.2. Fouling factors (coefficients), typical values

Coulson & Richardson Vol.6 ed.4



Tube dimensions

- Length (ft): 6, 8, 12, 16, 20, 24
- The optimum tube length to shell diameter: 5 to 10

Outside diameter (mm)	WW.	Wall	thickness	(mm)	
16	1.2	61.6	2.0		
20	_	1.6	2.0	2.6	
25	_	1.6	2.0	2.6	3.2
30		1.6	2.0	2.6	3.2
38			2.0	2.6	3.2
50	—		2.0	2.6	3.2

Table 12.3. Standard dimensions for steel tubes

Coulson & Richardson Vol.6 ed.4



Tube O.D. Inches	B.W.Cl. Gage	Thickness Inches	Internal Area Sg. Inch	Sq. Ft. External Surface Per Foot Length	Sq. Ft. Internal Sarface Per Foot Length	Weight Per F. Length Steel Lbs.*	Tuta: 1.D. Inches
144	24 26 27	0.028 0.022 0.018 0.016	0.0232 0.0250 0.0360 0.0375	0.0654 0.0654 0.0654 0.0654	0.0508 0.0539 0.0560 0.0571	0.054 0.045 0.040	0.194 0.206 0.214 0.218
78	18 20 22 24	0.049 0.035 0.028 0.022	0.0603 0.0731 0.0799 0.0560	0.0982 0.0982 0.0982 0.0982	0.0725 0.0798 0.0835 0.0967	0.171 0.127 0.164 0.085	0.277 0.305 0.319 0.031
1/2	16 18 20 22	0.065 0.049 0.035 0.028	0.1075 0.1269 0.1452 0.1546	0.1309 0.1309 0.1309 0.1309	0.0969 0.1052 0.1128 0.1162	0.902 0.236 0.174 0.141	0.370 0.402 0.430 0.444
6.8	12 13 14 15 16 17 10 19 20	2.109 2.095 2.083 2.072 2.065 2.065 2.049 2.049 2.049 2.049	0.1301 0.1406 0.1655 0.1817 0.1924 0.2005 0.2181 0.2399 0.2419	0.1636 0.1636 0.1636 0.1636 0.1636 0.1636 0.1636 0.1636 0.1636	2.1068 2.1139 2.1259 2.1259 2.1259 2.1333 2.1380 2.1416 2.1453	0.601 0.535 0.461 0.426 0.369 0.352 0.352 0.352 0.362 0.262 0.262	0.407 0.436 0.459 0.481 0.495 0.509 0.527 0.541 0.555
3/4	10 11 12 13 14 15 18 17 18 20	0.134 0.120 0.095 0.083 0.083 0.072 0.065 0.050 0.050 0.050	0.1625 0.2043 0.2223 0.2463 0.2679 0.2679 0.2679 0.2684 0.3019 0.3019 0.3157 0.5330 0.5632	0.1963 0.7963 0.1223 0.1222 0.1222 0.1965 0.1965 0.1963 0.1963 0.1963 0.1963	0.1262 0.1335 0.1466 0.1529 0.1587 0.1587 0.1683 0.1680 0.1707 0.1780	0.833 0.866 0.747 0.665 0.592 0.522 0.476 0.429 0.367 0.268	C.482 C.510 C.532 C.560 C.584 C.606 C.620 C.634 C.652 C.680
7.8	10 11 12 19 14 15 16 17 18 20	C. 134 C. 120 C. 109 C. 095 C. 089 C. 072 C. 065 C. 058 C. 049 C. 035	0.2894 0.3167 0.0090 0.0685 0.3948 0.4359 0.4359 0.4359 0.4525 0.4742 0.6090	0.2291 0.2291 0.2291 0.2291 0.2291 0.2291 0.2291 0.2291 0.2291 0.2291 0.2291	0.1589 0.1682 0.1723 0.1733 0.1836 0.1914 0.1967 0.2034 0.2034	1.062 0.549 0.653 0.752 0.703 0.618 0.563 0.507 0.433 0.514	0.607 0.635 0.665 0.685 0.709 0.731 0.745 0.759 0.759 0.777 0.805
1	8 10 11 12 13 14 16 16 16 20	0.165 0.134 0.120 0.095 0.095 0.072 0.063 0.072 0.065	0.3526 0.4208 0.4536 0.4633 0.5163 0.5463 0.5765 0.5945 0.6390 0.6793	0.2518 0.2518 0.2518 0.2518 0.2518 0.2518 0.2518 0.2518 0.2518 0.2518	0.1754 0.1915 0.1900 0.2047 0.2121 0.2183 0.2241 0.2278 0.2261 0.2261	1.473 1.241 1.129 1.038 0.010 0.614 0.614 0.614 0.614 0.650 0.498 0.501	0.670 0.732 0.762 0.810 0.834 0.856 0.856 0.902 0.902 0.930



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	I		· •	··· ·	$S_{\rm M}/M$	láų, M≓	Weight	
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Ξŧ.		17	1,475	12110	0.0499	E.6406	D 524	12 93
		13	1.240	1.4071	0.0493	0.0420	0.449	13.59
		13	1.007	1.2652	0.0493	0,0432	0 356	13.74
		20	0.869	1 8/209	00493	0.0443	0.329	14 10
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·		·4	2,109	1.7294 .	0.0596	0,0486	. 0.661	14.83
.		-5	1.829	1 8805	0.0556	0.00464	9.777	15 20
1		15	1651	1 9477	0.0536	0.0465	+ 4.705	15.75
			1.475	2.0050	0.0556	0.0506	9.F33	18,10
		-14	1.245	2 1542	3 2556	0 8576 2 0 0543	C 646 0.399	18.55
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		17	1 473	2.9193	0.0083	0.0005	0.794	1E.23
		13	1.240	3.0090	0.0693	0.0629	0.844	19.74
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.		1. 10	2.404	2.7149	0.0798	0.0584	1.847	16.59
		11	2,048	2 \$284	0.0729	C.0877	1 550	19.33
		12	7.760	\$ 3.0087	0.0/99	0.0624	1.545	19.86
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		· 10	1 245	1.1226	0.0798	0.020	0.741	22.91
ļ		20	0 969	4 3826	2 CTCE	0.3742	0.637	22.62
<u></u>						· · · ·	<u></u>	



DIMENSIONS OF WELDED AND SEAMLESS PIPE

NOMINAL	OUT-				2.61		NO	MINAL W	ALL THIC	KNESS FC	50			2235		
PIP2 SIZE	DIAM	SCHED SS*	SCHED: 10.9*	SCHED.	SCHED. 20	SCHED.	STAND ARD	SCHED.	SCHED.	STRONO	SCHED. 80	SCHED.	SCHED.	SCHED. 140	SCHED. 160	XX
94 94	0.405 0.540		0.049				830.0 830.0	0.048		0.095 0.119	0.095		(a)	1	12	
86 1/2	0.675	0.005	0.065				0.091 0.109	0.091		0.128 0.74/	0.126	1.1.1		SALL.	0.188	0.294
, ^{3%}	1,050	0.085	0.083				C.113 C 123	0.113 0.133		0,154 0,175	0.154				0.219	0.308
134 135	1.650	0.065	0.109 0.109			5	0.140	0.140		0.200	0.191	- ()		1 20	0.250	0.3 #2
2 7%	2.375 7.875	0.065	0.109				0.154 0.203	0.154 0.203		0.278	0.218				0.344	0.434
с зул	3.5 4.0	0.063 0.063	0.120 0.120				0.316 0.228	0.216	-	0.300	0.300				0.438	0.600
4	4 5 5.563	0.083	0.120 0.134			1-+ W	0.237 0.258	0.737 0.258		0.337 0.375	0.337 0.375		0.438		0.531 0.625	0.674
0 8	0 025 8 025	0.109 0.109	0.134 0.148		0.250	0.277	4 280 0.322	0.280	0.406	0.432 0.500	0.432	0.594	0.562	0.812	0.719	0.864
10 12	10.75 12.75	0.134	0.165		0.250	0.307 0.330	0.365 0.375	0.90a	0.500 0.562	0.500 0.500	0.594	0.719 0.844	0.844	1.000	1.125	1.000
14 O.D. 16 O.D.	14.0 16.0	0.156	0.188	0.250	0.312	0.375	0.375	0.438 0.500	0.094	0.500 0.500	0.750	0.935	1.094	1.250	1.406	
18 O.D. 20 O.D.	18.0 20.0	0.165 0.188	0.138	0.250	0.312 0.375	0.438	0.375	0.562 0.594	0.750	0.500	0.938	1.156	1.375	1.562	1.781	
33 D.D. 24 D.D.	22.0 24.0	1750570	0.218	0.250	0.375 0.375	0.500	0.375	0.683	0.875	0.500	1.125 1.218	1.325	1.625 1.812	1.875 2.062	2.125 2.344	
26 D.D. 26 D.D.	28.0 28.0			0.312	0.300	0.625	0.375			0.50C 0.500			15			1
30 O.D. 32 O.D.	30.0 32.0	0.250	0.313	0.312	0.500	0.625	0.375	0.688		0.50C 0.50C		1 - E 1 - E 1	Ň.,		1	1.14.81
34 O.D. 36 O.D.	34.0 36.0			0.312 0.312	0.500	0.625	0.375 0.375	0.688 0.750		0.50C 0.500						
41 O.D.	42.0			22.1	1.44	(eee)	0.375			0.500		+1	1.1	1000	1000	

All dimensions are given in inches.

The decimal thicknesses listed for the respective pipe sizes represent their nominal or average wall dimensions. The actual thicknesses may be as much as 125% under the nominal thicknesses way be not reacting thicknesses chown in bold face are more reactly available.

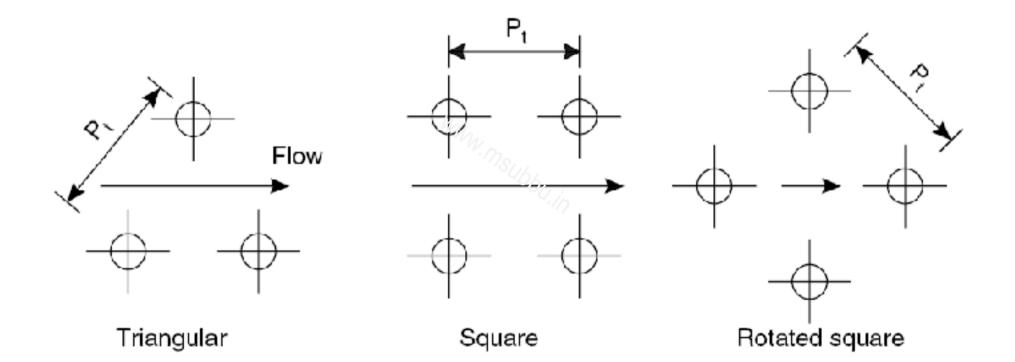
 Schedules 55 and 105 are available in certasion resistant materials and Schedule 105 is pice available in caroon stati.

 Thicknesses shown in Halics are available also in stainless steel under the designation Schedule 406.

§Thicknesses shown in italics are available also in stamless steel under the designation Schedule 805.



Tube Patterns



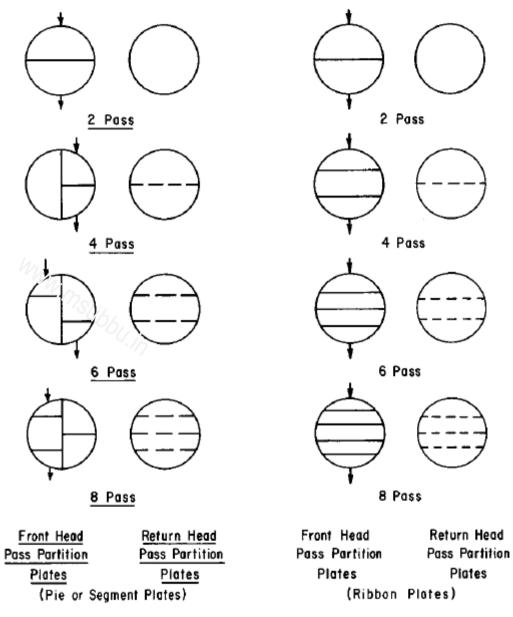


Tube side passes

- Practical construction limits the number of tube-side passes to 8—10, although a larger number of passes may be used on special designs
- Even number of passes are preferred
- The higher the number of passes, the more expensive the unit



Tube Side Passes





Shell Diameter

$$D_b = d_o \left(\frac{N_t}{K_1}\right)^{1/n_1}$$

where N_t = number of tubes,

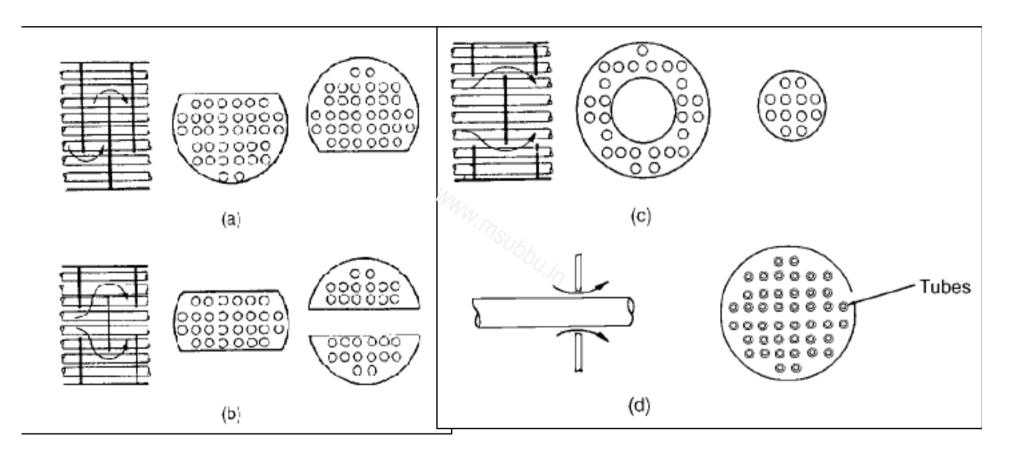
 $D_b =$ bundle diameter, mm,

 $d_o =$ tube outside diameter, mm.

Triangular pitch	, $p_t = 1.25 d_o$	n _{SU/}	54		
No. passes	1	2	·//4	6	8
$egin{array}{c} K_1 \ n_1 \end{array}$	0.319 2.142	0.249 2.207	0.175 2.285	0.0743 2.499	0.0365 2.675
Square pitch, p	$= 1.25 d_o$				
No. passes	1	2	4	6	8
$egin{array}{c} K_1 \ n_1 \end{array}$	0.215 2.207	0.156 2.291	0.158 2.263	0.0402 2.617	0.0331 2.643



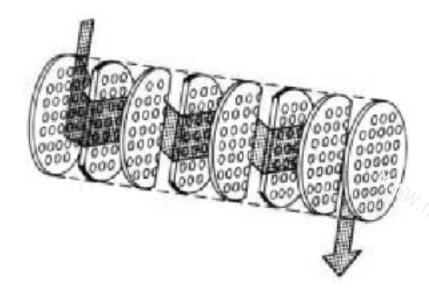
Baffles

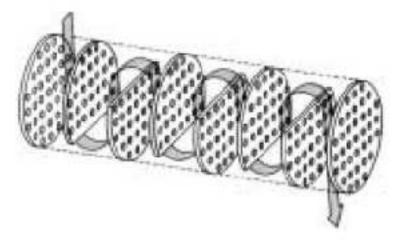


Types of baffle used in shell and tube heat exchangers. (a) Segmental (b) Segmental and strip (c) Disc and doughnut (d) Orifice



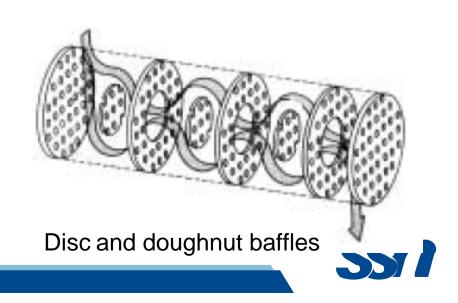
Baffles





Horizontal cut segmental baffles

Vertical cut segmental baffles



Fluid Allocation

- **Corrosion**: Fewer costly alloy components are needed if the corrosive fluid is inside the tubes. Corrosive fluid cannot be sent in the shell side, since the shell side fluid will affect both shell and tubes.
- **Fouling**: Placing the fouling fluid inside the tubes allow better velocity control; increased velocities tend to reduce fouling. Straight tubes allow mechanical cleaning without removing the tube bundle.
- **Temperature & Pressure**: For high temperature / pressure services requiring special or expensive alloy materials, fewer alloy components are needed when hot fluid is placed within the tubes
- Flow rate: Placing the fluid with the lower flow rate on the shell side usually results in a more economical design. Turbulence exists on the shell side at much lower velocities than within the tubes.



Fluid Velocities

- Liquids:
 - Tube side: 1 2 m/s; maximum 4 m/s if required to reduce fouling
 - Shell side: 0.3 1 m/s
- Gases:
 - Atmospheric pressure: 10 30 m/s



Tube side heat transfer coefficient

(turbulent flow)

$$Nu = CRe^{0.8}Pr^{0.33} \left(\frac{\mu}{\mu_w}\right)^{0.14}$$

where C = 0.021 for gases,

= 0.023 for non-viscous liquids,

= 0.027 for viscous liquids.

where Nu = Nusselt number = $(h_i d_e/k_f)$, Re = Reynolds number = $(\rho u_i d_e/\mu) = (G_i d_e/\mu)$, Pr = Prandtl number = $(C_p \mu/k_f)$ and: h_i = inside coefficient, W/m²°C, d_e = equivalent (or hydraulic mean) diameter, m

 $d_e = \frac{4 \times \text{cross-sectional area for flow}}{\text{wetted perimeter}} = d_i$ for tubes,

 $u_t =$ fluid velocity, m/s,

 $k_f =$ fluid thermal conductivity, W/m°C,

 G_t = mass velocity, mass flow per unit area, kg/m²s,

 μ = fluid viscosity at the bulk fluid temperature, Ns/m²,

 $\mu_w =$ fluid viscosity at the wall,

 C_p = fluid specific heat, heat capacity, J/kg°C.



Tube side heat transfer coefficient (laminar flow)

$$Nu = 1.86(RePr)^{0.33} \left(\frac{d_e}{L}\right)^{0.33} \left(\frac{\mu}{\mu_w}\right)^{0.14}$$



Shell side

• Cross flow area (A_s)

$$A_s = \frac{(p_t - d_o)D_s l_B}{p_t}$$

where p_t = tube pitch,

 d_o = tube outside diameter,

 D_s = shell inside diameter, m,

 $l_B =$ baffle spacing, m.

• Shell side mass velocity and linear velocity

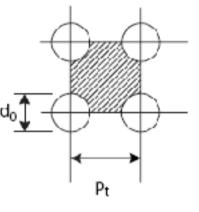
$$G_s = \frac{W_s}{A_s}$$
$$u_s = \frac{G_s}{\rho}$$



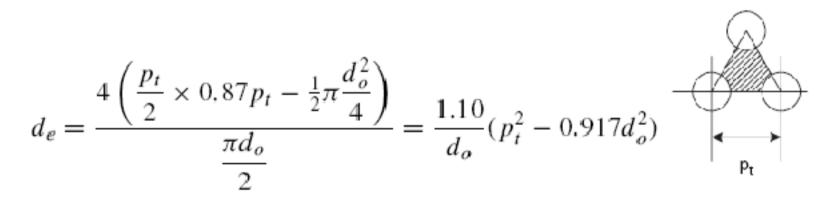
Shell side equivalent diameter

• Square pitch

$$d_e = \frac{4\left(\frac{p_t^2 - \pi d_o^2}{4}\right)}{\pi d_o} = \frac{1.27}{d_o}(p_t^2 - 0.785d_o^2)$$



• Triangular pitch





Shell side heat transfer coefficient

$$Re = \frac{G_s d_e}{\mu} = \frac{u_s d_e \rho}{\mu}$$
$$Nu = \frac{h_s d_e}{k_f} = j_h Re P r^{1/3} \left(\frac{\mu}{\mu_w}\right)^{0.14}$$



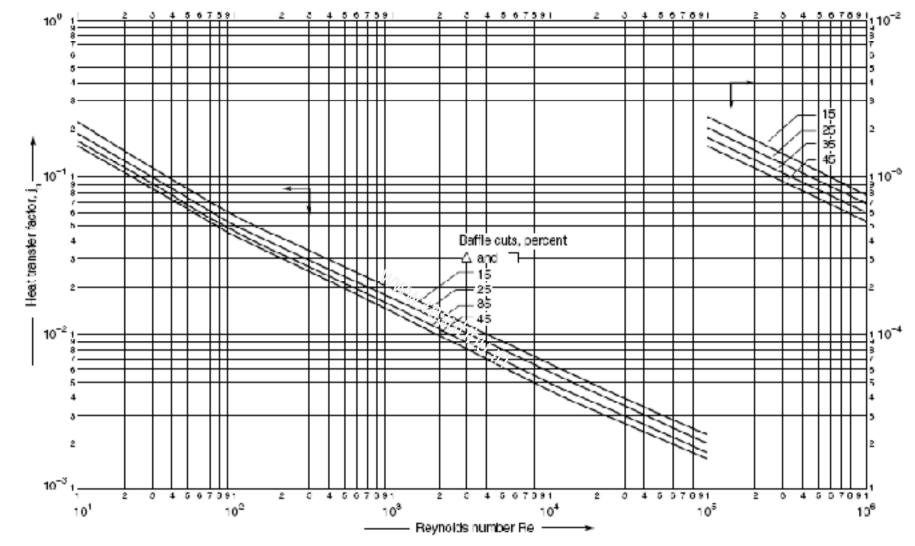


Figure 12.29. Shell-side heat-transfer factors, segmental baffles

Coulson & Richardon Vol.6 ed.4



Pressure drop calculations

 $f = 0.079 Re^{-0.25}$

• Tube side:

$$\Delta P_t = N_p \left[\frac{4f\mathbb{Z}}{D} + 2.5 \right] \frac{\rho v_t^2}{2}$$

• Shell side:

$$\Delta P_s = \left[\frac{4fL}{d_e}\frac{D_s}{l_B}\right]\frac{\rho v_s^2}{2}$$



Allowable Pressure Drop

- Liquids: 35 70 kN/m²
- Gases and vapors:
 - High vacuum: $0.4 0.8 \text{ kN/m}^2$
 - Medium vacuum: 0.1 x absolute pressure
 - 1 to 2 bar: 0.5 x system gauge pressure



Design Codes

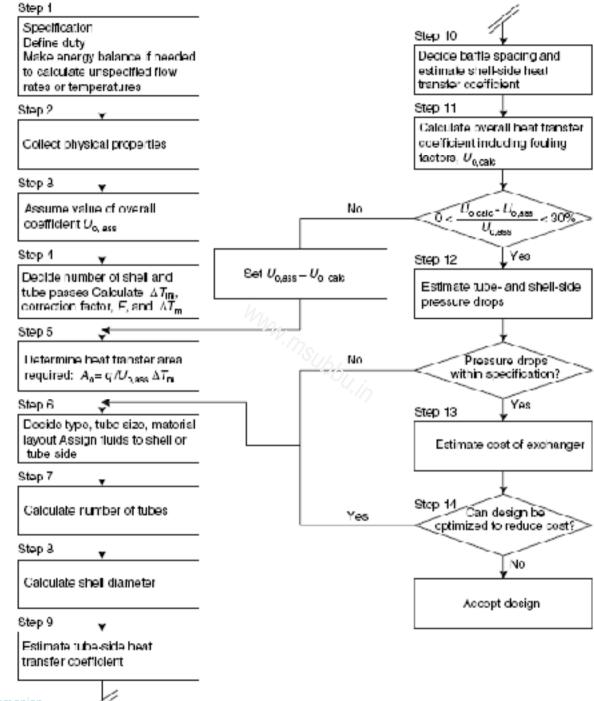
- Standards developed by Tubular Exchanger Manufacturers Association, USA (TEMA) are universally used for design of shell and tube heat exchangers.
- Equivalent Indian code is IS: 4503
- These codes specify the standard sizes of shell, tubes, etc., and also maximum allowable baffle spacing, minimum tube sheet thickness, baffle thickness, number of tie-rods required, etc.



Design Procedure

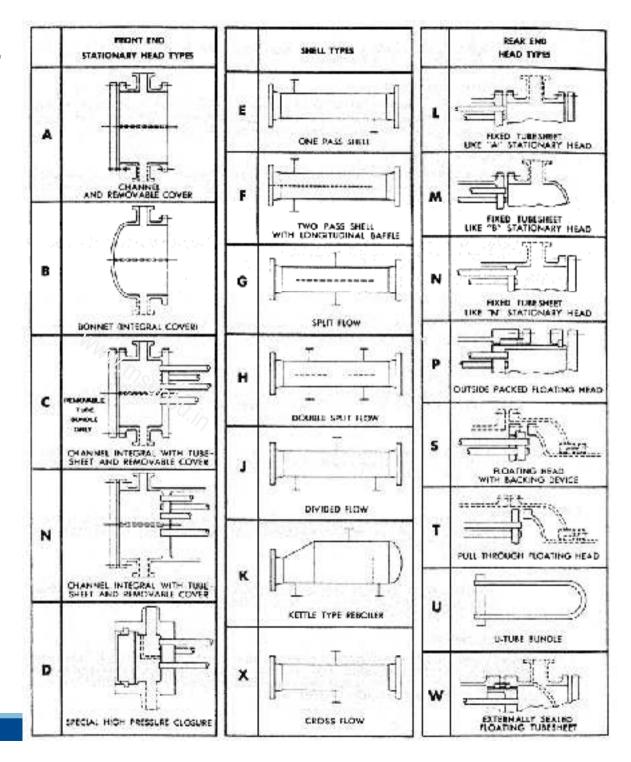
- 1. Define the duty: heat-transfer rate, fluid flow-rates, temperatures.
- Collect together the fluid physical properties required: density, viscosity, thermal conductivity.
- 3. Decide on the type of exchanger to be used.
- 4. Select a trial value for the overall coefficient, U.
- 5. Calculate the mean temperature difference, ΔT_m .
- 6. Calculate the area required from equation 1.
- 7. Decide the exchanger layout.
- 8. Calculate the individual coefficients.
- 9. Calculate the overall coefficient and compare with the trial value. If the calculated value differs significantly from the estimated value, substitute the calculated for the estimated value and return to step 6.
- Calculate the exchanger pressure drop; if unsatisfactory return to steps 7 or 4 or 3, in that order of preference.
- 11. Optimise the design: repeat steps 4 to 10, as necessary, to determine the cheapest exchanger that will satisfy the duty. Usually this will be the one with the smallest area.





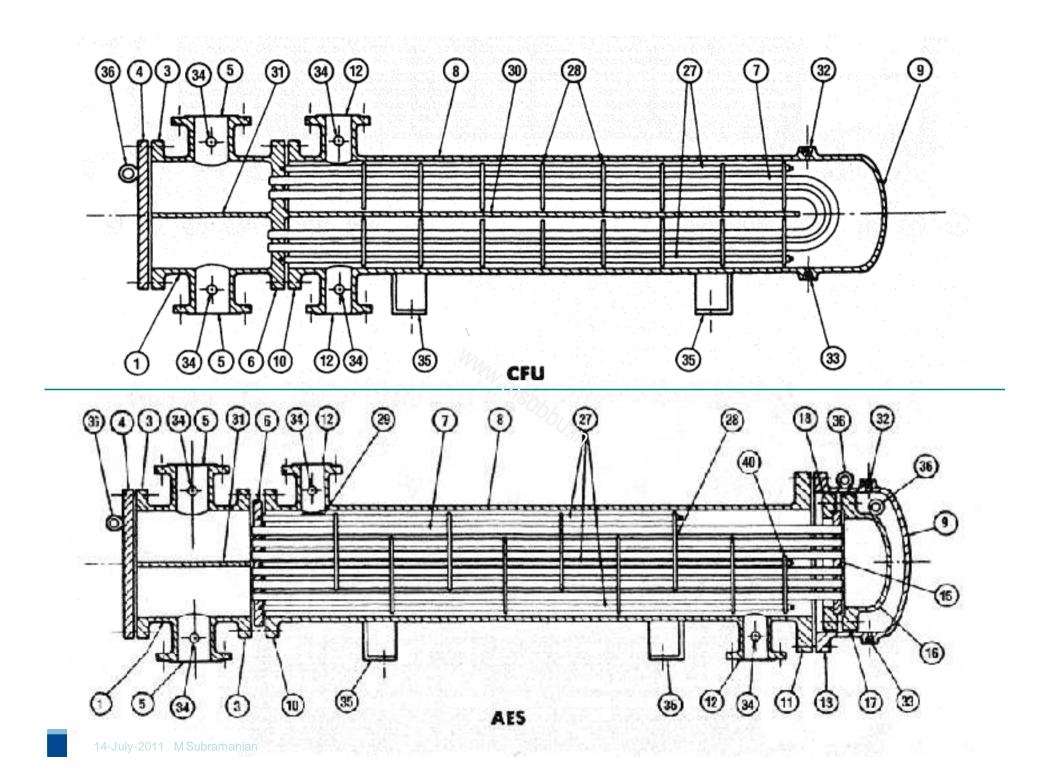


Nomenclature for Heat Exchanger Components



TEMA

14-July-2011 M Subramanian



Typical Parts of a Heat Exchanger

 Stationary Head-Channel 2 Stationary Head-Bonnet 3. Stationary Head Flange-Channel or Bonnet 4 Channel Cover 5 Stationary Head Nozzle 6 Stationary Tubesheet 7. Tubes 8. Shell 9 Shell Cover 10. Shell Flange-Stationary Head End 11. Shell Flange-Rear Head End 12 Shell Nozzle 13 Shell Cover Flange 14. Expansion Joint 15 Floating Tubesheet 16. Floating Head Cover 17. Floating Head Cover Flange 18. Floating Head Backing Device 19. Split Shear Ring 20. Slip-on Backing Flange

21. Floating Head Cover-External 22. Floating Tubesheet Skirt 23. Packing Box 24. Packing 25. Packing Gland 26. Lantern Ring 27. Tierods and Spacers 28. Transverse Baffles or Support Plates 29. Impingement Plate 30. Longitudinal Battle 31. Pass Partition 32. Vent Connection 33. Drain Connection 34. Instrument Connection 35. Support Saddle 36. Lifting Lug 37. Support Bracket 38. Weir 39. Liquid Level Connection

40. Floating Head Support



HEAT EXCHANGER SPECIFICATION SHEET

C INVESTIGATION OF CONTRACTOR OF		Job No					
Cutomer			Reference No.				
Address	1	Propor					
Plant Location		Cate	Rev				
Service of Unit	1.	Rom M					
	e'Vert;		ctod in Para				
Suf/Uni (Gross/Eff.) Sa	Ft_Shalk/070		heil (Gross/Eff.)	Sq H			
	PERFORM	ANCE OF ONE UNIT	S. Star Star Hand	120			
Fluid Allocation		Shell Side	Tut	ine Side			
Fluid Name	35						
Fluid Quantity Tetal	LIXHr			- Ante-			
Vepar (In/Out)	1.1		1/- e= -=	1			
Liquid	11-1-1- G			1			
Skam Water		1.0		1			
Water							
Noncondensablo				-			
Temperature (In/Out)	op			1 1 2 5 - 5 4 2 - 2			
Specific Gravity	anay Maria						
Viscos by, Liquid	Dø						
Molecular Weight, Vapor				1			
Malocular Weight, Nersondensable	and the second		100 C				
	Sturi Lb 9F		-				
Thermal Conductivity Blu FL()	Ir Sej Pt "F			A LEASE HOLL - NA			
	715 @ 9F	A		1			
Inist Pressure	Pata						
Vessity	F17 Sov	110					
Pressure Drop, Allow, /Calc.	Pai			1			
	°F/Bla						
Heat Exchanged	in the second	Dia / Hetal D. (Come	ted)	5			
Transfer Rate, Service		Clean	1.1.1.	Biu / Hr Sq Ft 'F			
	ION OF ONE SHE	and the second se	Ekeich (Sundia	Nozzie Orieniation)			
	Shell Side	Tube Side					
Design / Test Pressure Psig			1.5				
Design Toma, Max.Min *F No. Passes per Shell							
No. Passes per Shell							
Corresion Allewance In			2				
Connections In							
Stza é Out	14 C 14 C						
Rating Intermediate			L. King and A.				
Tube No. OD in(Tilk (Min/Avg)	In;Leng		in in ≼-249-±4	60 - 50 - 45			
lube Type	00 1	Material	1	a) (Remov)			
Shel ID	QU 1	n Shell Cover	(inte	g.) (proemary)			
Channe or Bornet		Channel Cover					
Tubeshoof Stationary		Tubosheet-Floating					
Floating Head Cover		Impingement Protect	non	r int in			
Baffee-Cross Type		%Cut (Olemi/Area)	Spacing: o/c	nint in			
BaFes-Long	C. B. C. d	Seal Type					
Supports Tube	U-Bend	71	Туре				
Bypass Saal Arrangement		Tube-to-Tubeshert .	em				
Expansion Joint	D	Туре	In and to d				
py-Iniol Nozzle	Burdie Entranc		Bundle Exit				
Cardenty-Shad Side		Tube Side					
Floating Heat		and the second second					
Code Requirements	Filed with V		TEMA Class	and the state of the			
allerate Shell			Bundle	11			

