

CH2303 Chemical Engineering Thermodynamics I

Unit – IV

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Thermodynamic Property Relations

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Contents

- Measurable quantities, basic energy relations, Maxwell relations,
- Thermodynamic formulations to calculate enthalpy, internal energy and entropy as function of pressure and temperature,
- Other formulations involving C_p and C_v , complex thermodynamic formulations,

Mathematical Relations

$$F = F(x, y)$$

$$dF = \left(\frac{\partial F}{\partial x} \right)_y dx + \left(\frac{\partial F}{\partial y} \right)_x dy$$

$$dF = M dx + N dy$$

$$\frac{\partial^2 F}{\partial y \partial x} = \frac{\partial^2 F}{\partial x \partial y}$$

exactness criteria:

$$\left(\frac{\partial M}{\partial y} \right)_x = \left(\frac{\partial N}{\partial x} \right)_y$$

Cyclic Relation Rule

For the function in the variables x, y & z

$$\left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial z}\right)_x \left(\frac{\partial z}{\partial x}\right)_y = -1$$

Other Relations of Importance

$$\left(\frac{\partial x}{\partial y}\right)_z = \frac{1}{\left(\frac{\partial y}{\partial x}\right)_z}$$

fundamental property relations:

$$dU = TdS - PdV$$

$$dH = VdP + TdS$$

$$dG = -SdT + VdP$$

$$dA = -PdV - SdT$$

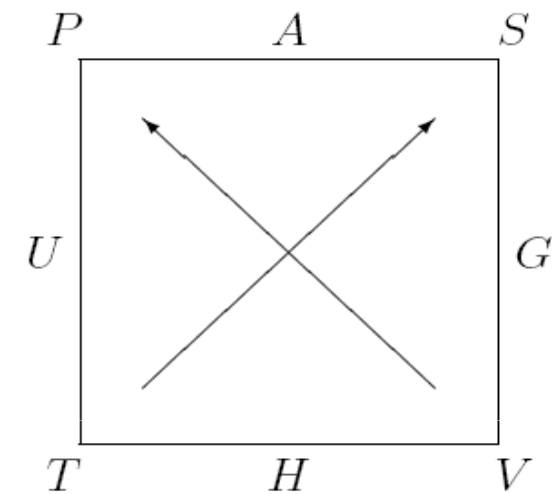
Maxwell Relations

$$\left(\frac{\partial T}{\partial V}\right)_S = -\left(\frac{\partial P}{\partial S}\right)_V$$

$$\left(\frac{\partial V}{\partial S}\right)_P = \left(\frac{\partial T}{\partial P}\right)_S$$

$$\left(\frac{\partial S}{\partial P}\right)_T = -\left(\frac{\partial V}{\partial T}\right)_P$$

$$\left(\frac{\partial P}{\partial T}\right)_V = \left(\frac{\partial S}{\partial V}\right)_T$$



PASGVHTU

$$\left(\frac{\partial U}{\partial T} \right)_V = C_V$$

$$\left(\frac{\partial H}{\partial T} \right)_P = C_P$$

$$V = V(T, P)$$

$$\frac{dV}{V} = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P dT + \frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T dP$$

$$\frac{dV}{V} = \beta dT - \kappa dP$$

$$\beta = \text{Volume expansivity} = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P$$

$$\kappa = \text{Isothermal compressibility} = -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T$$

Relations for dU

$$U = U(T, V)$$

$$dU = C_V dT + \left[T \left(\frac{\partial P}{\partial T} \right)_V - P \right] dV$$

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Relations for dH

$$H = H(T, P)$$

$$dH = C_P dT + \left[V - T \left(\frac{\partial V}{\partial T} \right)_P \right] dP$$

Relations for dS

$$\left(\frac{\partial S}{\partial T}\right)_V = \frac{C_V}{T}$$

$$\left(\frac{\partial S}{\partial T}\right)_P = \frac{C_P}{T}$$

$$S = S(T, V)$$

$$dS = \frac{C_V}{T}dT + \left(\frac{\partial P}{\partial T}\right)_V dV$$

$$S = S(T, P)$$

$$dS = \frac{C_P}{T}dT - \left(\frac{\partial V}{\partial T}\right)_P dP$$

Relations for Specific heats

$$C_P = T \left(\frac{\partial P}{\partial T} \right)_S \left(\frac{\partial V}{\partial T} \right)_P$$

$$C_V = -T \left(\frac{\partial P}{\partial T} \right)_V \left(\frac{\partial V}{\partial T} \right)_S$$

$$C_P - C_V = -T \left(\frac{\partial P}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_P^2$$

$$\frac{C_P}{C_V} = \frac{(\partial P / \partial V)_S}{(\partial P / \partial V)_T}$$

$$\left(\frac{\partial C_P}{\partial P} \right)_T = -T \left(\frac{\partial^2 V}{\partial T^2} \right)_P$$

$$\left(\frac{\partial C_V}{\partial V} \right)_T = T \left(\frac{\partial^2 P}{\partial T^2} \right)_V$$

Two-phase Systems

$$d(nG) = (nV)dP - (nS)dT$$

During phase change T and P remains constant. Therefore, $d(nG) = 0$.
Since $dn \neq 0$, $dG = 0$.

For two phases α and β of a pure species coexisting at equilibrium:

$$G^\alpha = G^\beta$$

$$dG^\alpha = dG^\beta$$

$$\frac{dP^{\text{sat}}}{dT} = \frac{\Delta S^{\alpha\beta}}{\Delta V^{\alpha\beta}}$$

Clapeyron equation

$$\frac{dP^{\text{sat}}}{dT} = \frac{\Delta H^{\alpha\beta}}{T\Delta V^{\alpha\beta}}$$

Clausius-Clapeyron equation

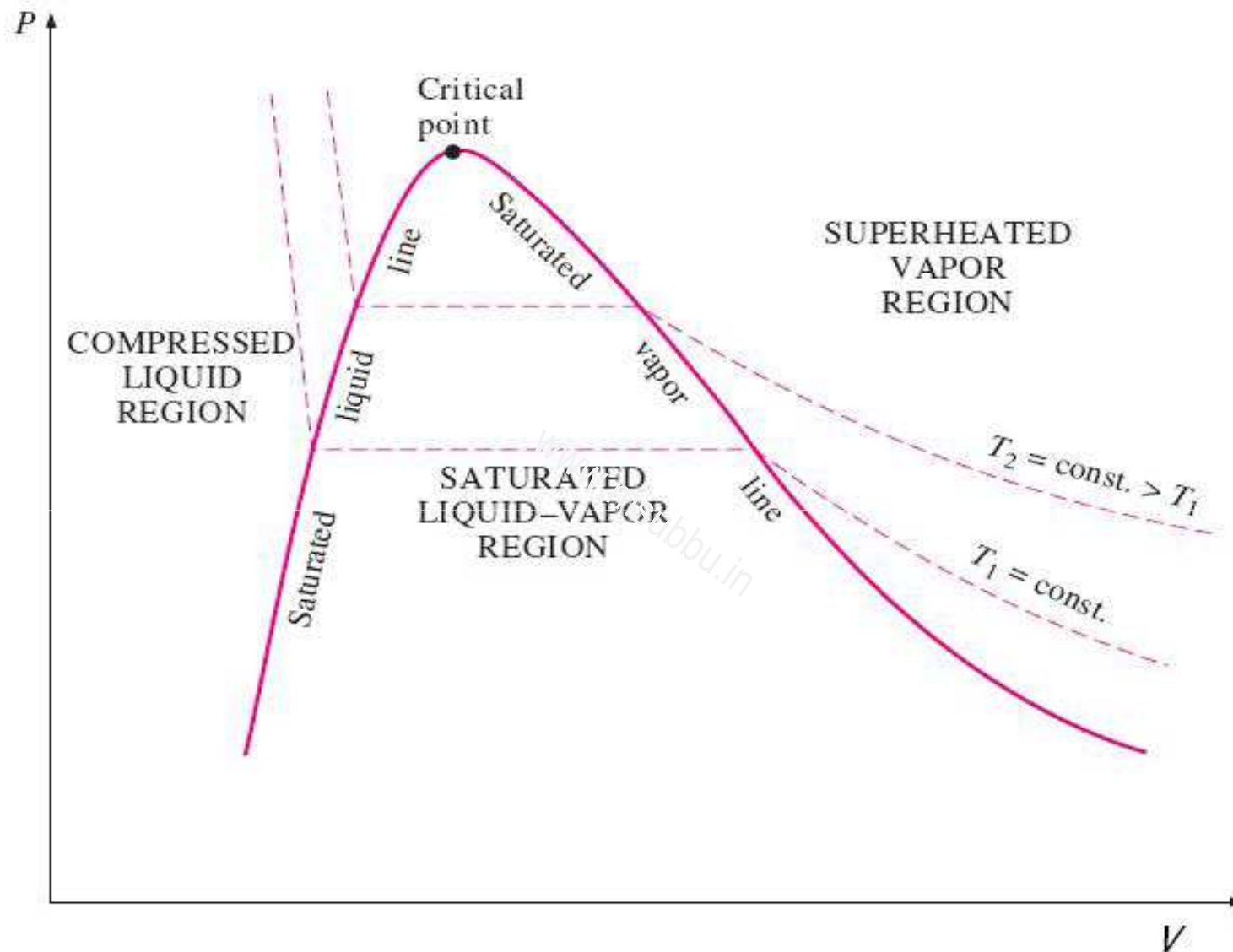
$$\ln \frac{P_2^{\text{sat}}}{P_1^{\text{sat}}} = \frac{\Delta H}{R} \left(\frac{1}{T_1} - \frac{1}{T_2} \right)$$

From Clausius-Clapeyron equation

$$\ln P^{\text{sat}} = A - \frac{B}{T}$$

A satisfactory relation given by *Antoine* is of the form

$$\ln P^{\text{sat}} = A - \frac{B}{T + C}$$



Steam tables

Temp. °C <i>T</i>	Press. kPa, MPa <i>P</i>	Specific Volume, m ³ /kg		Internal Energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg	
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Evap. <i>u_{fg}</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Evap. <i>h_{fg}</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Evap. <i>s_{fg}</i>
0.01 TP	0.6113	0.001000	206.132	0.00	2375.3	2375.3	0.00	2501.3	2501.3	0.0000	9.1562
5	0.8721	0.001000	147.118	20.97	2361.3	2382.2	20.98	2489.6	2510.5	0.0761	8.9496
10	1.2276	0.001000	106.377	41.99	2347.2	2389.2	41.99	2477.7	2519.7	0.1510	8.7498
15	1.7051	0.001001	77.925	62.98	2333.1	2396.0	62.98	2465.9	2528.9	0.2245	8.5569
20	2.3385	0.001002	57.790	83.94	2319.0	2402.9	83.94	2454.1	2538.1	0.2966	8.3706
25	3.1691	0.001003	43.359	104.86	2304.9	2409.8	104.87	2442.3	2547.2	0.3673	8.1905
30	4.2461	0.001004	32.893	125.77	2290.8	2416.6	125.77	2430.5	2556.2	0.4369	8.0164
35	5.6280	0.001006	25.216	146.65	2276.7	2423.4	146.66	2418.6	2565.3	0.5052	7.8478
40	7.3837	0.001008	19.523	167.53	2262.6	2430.1	167.54	2406.7	2574.3	0.5724	7.6845
.....											
75	38.578	0.001026	4.131	313.87	2162.0	2475.9	313.91	2321.4	2635.3	1.0154	6.6670
80	47.390	0.001029	3.407	334.84	2147.4	2482.2	334.88	2308.8	2643.7	1.0752	6.5369
85	57.834	0.001032	2.828	355.82	2132.6	2488.4	355.88	2296.0	2651.9	1.1342	6.4102
90	70.139	0.001036	2.361	376.82	2117.7	2494.5	376.90	2283.2	2660.1	1.1924	6.2866
95	84.554	0.001040	1.982	397.86	2102.7	2500.6	397.94	2270.2	2668.1	1.2500	6.1659
100	101.35	0.001044	1.6729	418.91	2087.6	2506.5	419.02	2257.0	2676.0	1.3068	6.0480
.....											
340	14.586	0.001038	0.010797	1570.26	894.3	2464.5	1594.15	1027.9	2622.0	3.6593	1.6763
350	16.514	0.001740	0.008813	1641.81	776.6	2418.4	1670.54	893.4	2563.9	3.7776	1.4336
360	18.651	0.001892	0.006945	1725.19	626.3	2351.5	1760.48	720.5	2481.0	3.9146	1.1379
370	21.028	0.002213	0.004926	1843.84	384.7	2228.5	1890.37	441.8	2332.1	4.1104	0.6868
374.1 CP	22.089	0.003155	0.003155	2029.58	0	2029.6	2099.26	0	2099.3	4.4297	0

Single-phase tables

TABLE A.1.3SI Superheated Vapor Water (SI Units)

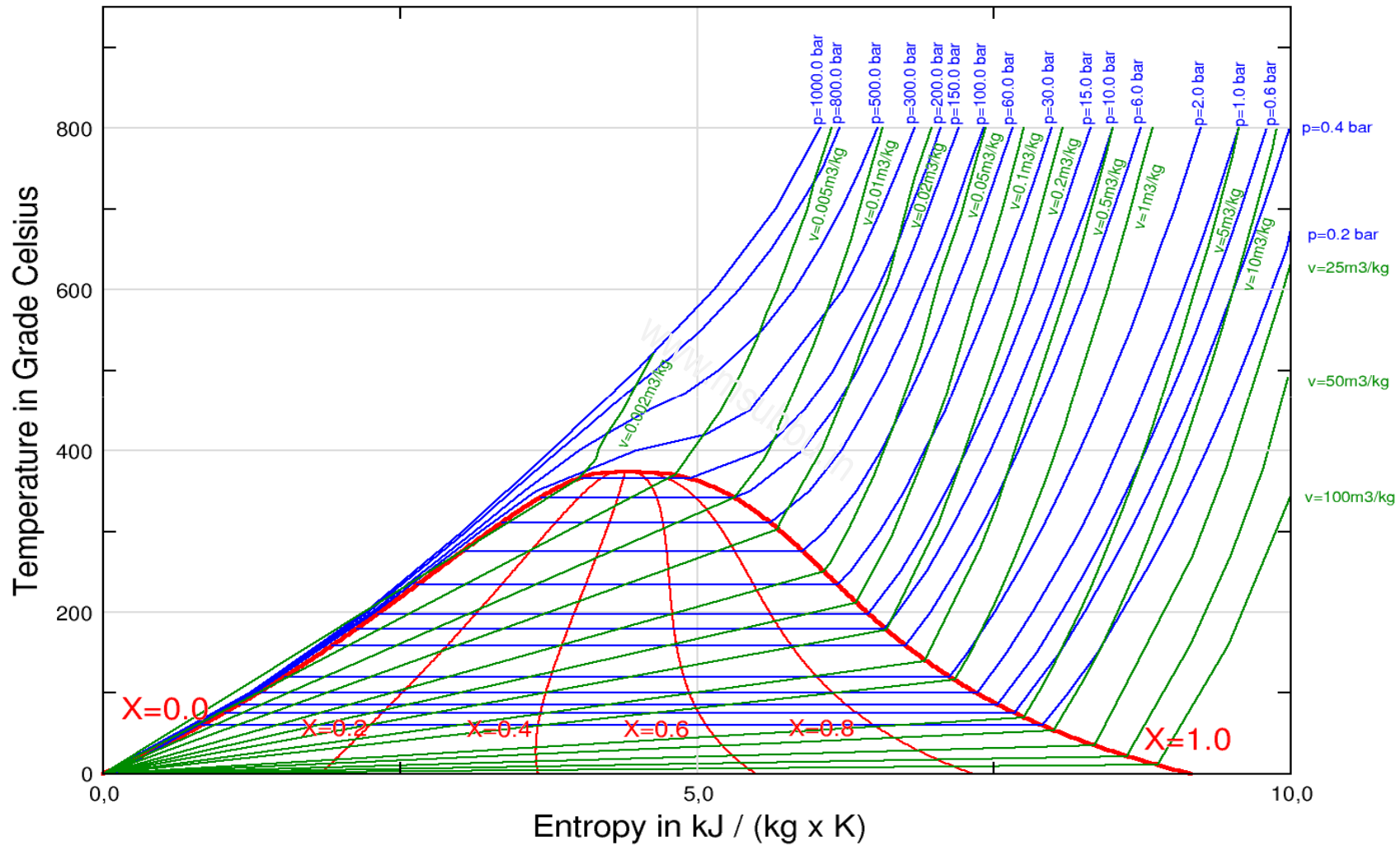
<i>T</i>	<i>P</i> = 10 kPa (45.81)				<i>P</i> = 50 kPa (81.33)			
	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>
Sat.	14.674	2437.9	2584.6	8.1501	3.240	2483.8	2645.9	7.593
50	14.869	2443.9	2592.6	8.1749	—	—	—	—
100	17.196	2515.5	2687.5	8.4479	3.418	2511.6	2682.5	7.694
150	19.513	2587.9	2783.0	8.6881	3.889	2585.6	2780.1	7.940
200	21.825	2661.3	2879.5	8.9037	4.356	2659.8	2877.6	8.157
250	24.136	2736.0	2977.3	9.1002	4.821	2735.0	2976.0	8.355
300	26.445	2812.1	3076.5	9.2812	5.284	2811.3	3075.5	8.537

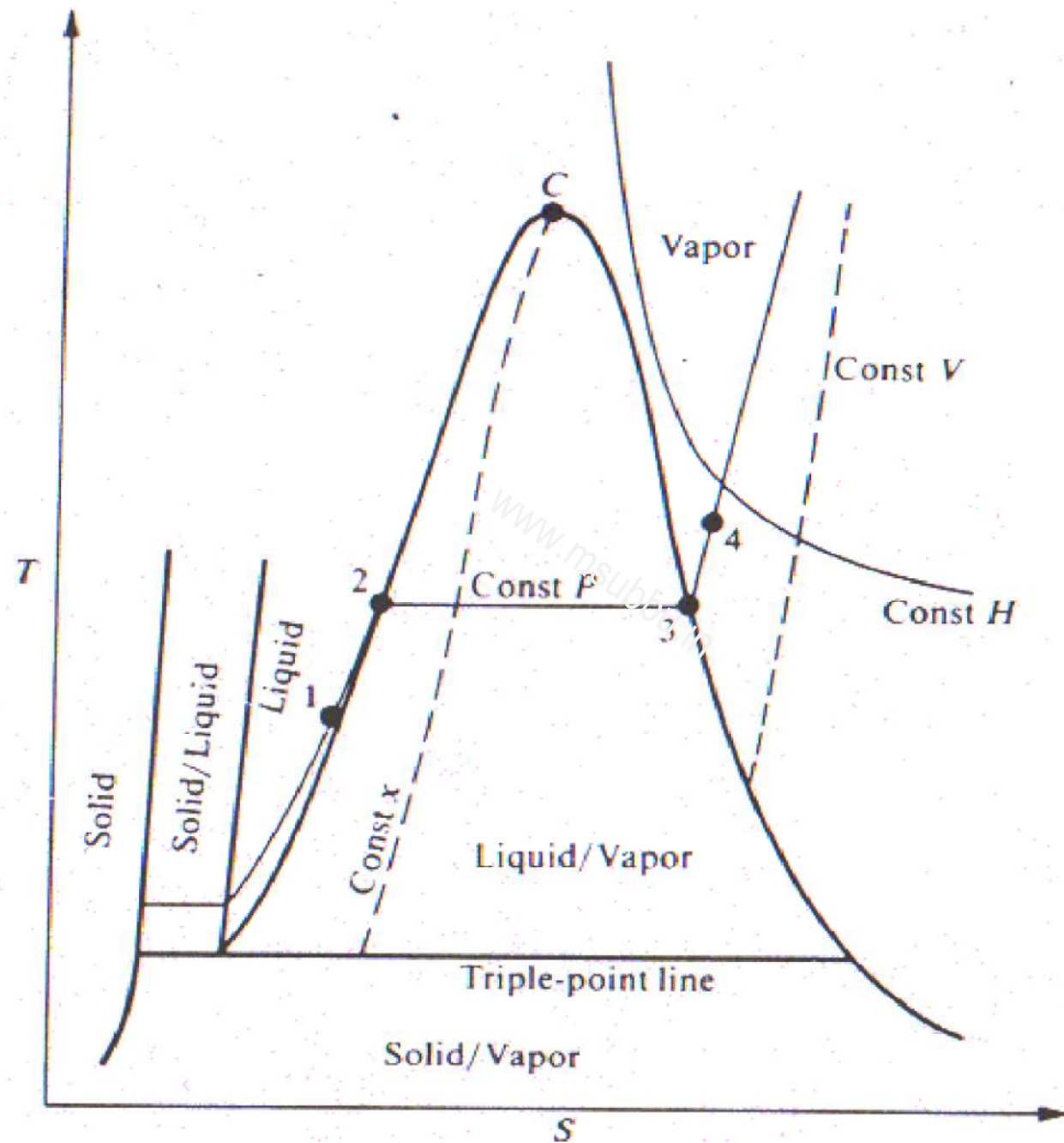
TABLE A.1.4SI Compressed Liquid Water (SI Units)

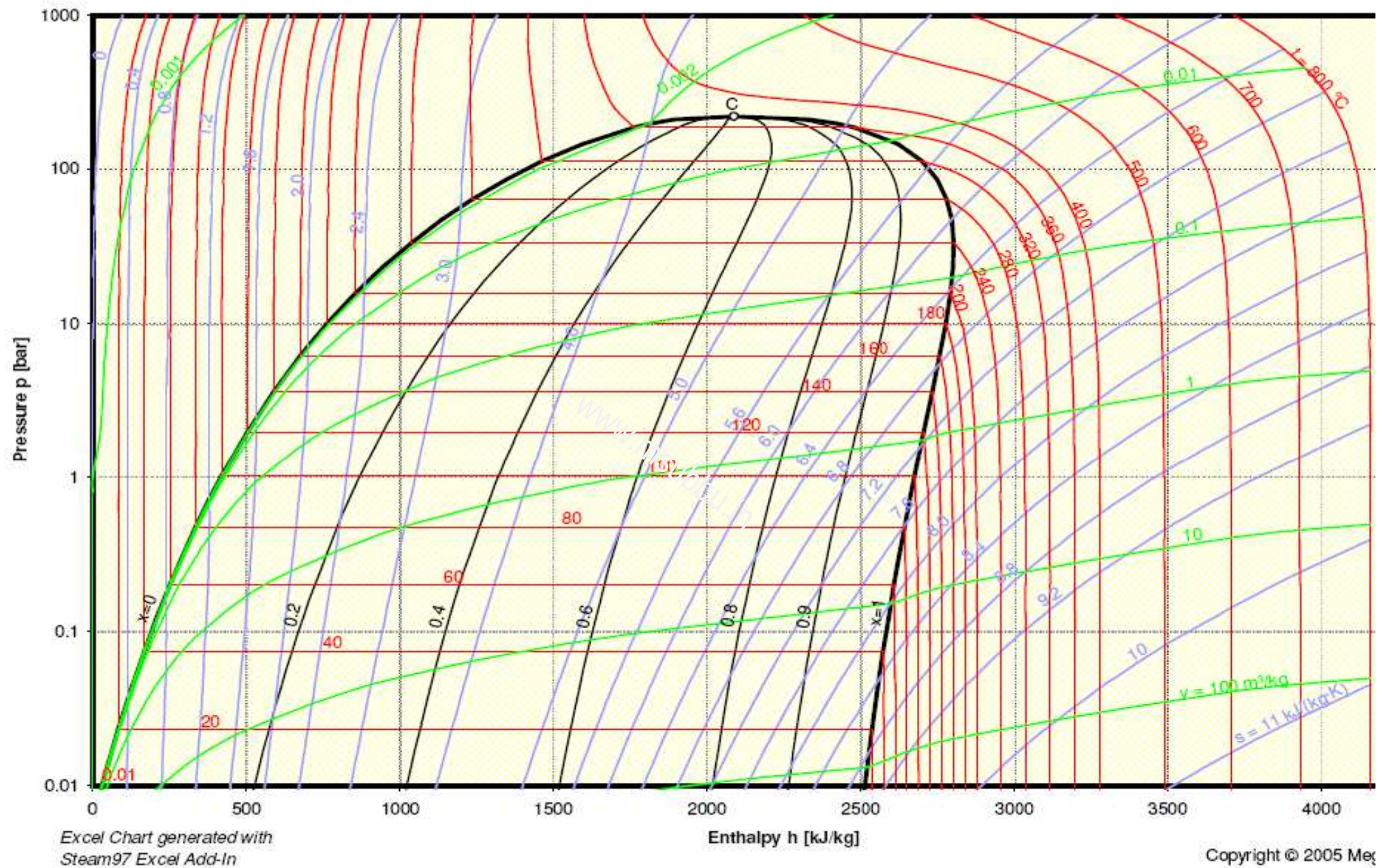
<i>T</i>	<i>P</i> = 5.00 MPa (263.99)				<i>P</i> = 10.00 MPa (311.06)			
	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>
Sat.	.0012859	1147.78	1154.21	2.9201	.0014524	1393.00	1407.53	3.359
0	.0009977	0.03	5.02	0.0001	.0009952	0.10	10.05	0.000
20	.0009995	83.64	88.64	0.2955	.0009972	83.35	93.32	0.294
40	.0010056	166.93	171.95	0.5705	.0010034	166.33	176.36	0.561
60	.0010149	250.21	255.28	0.8284	.0010127	249.34	259.47	0.821
80	.0010268	333.69	338.83	1.0719	.0010245	332.56	342.81	1.061
100	.0010410	417.50	422.71	1.3030	.0010385	416.09	426.48	1.291

Water Steam

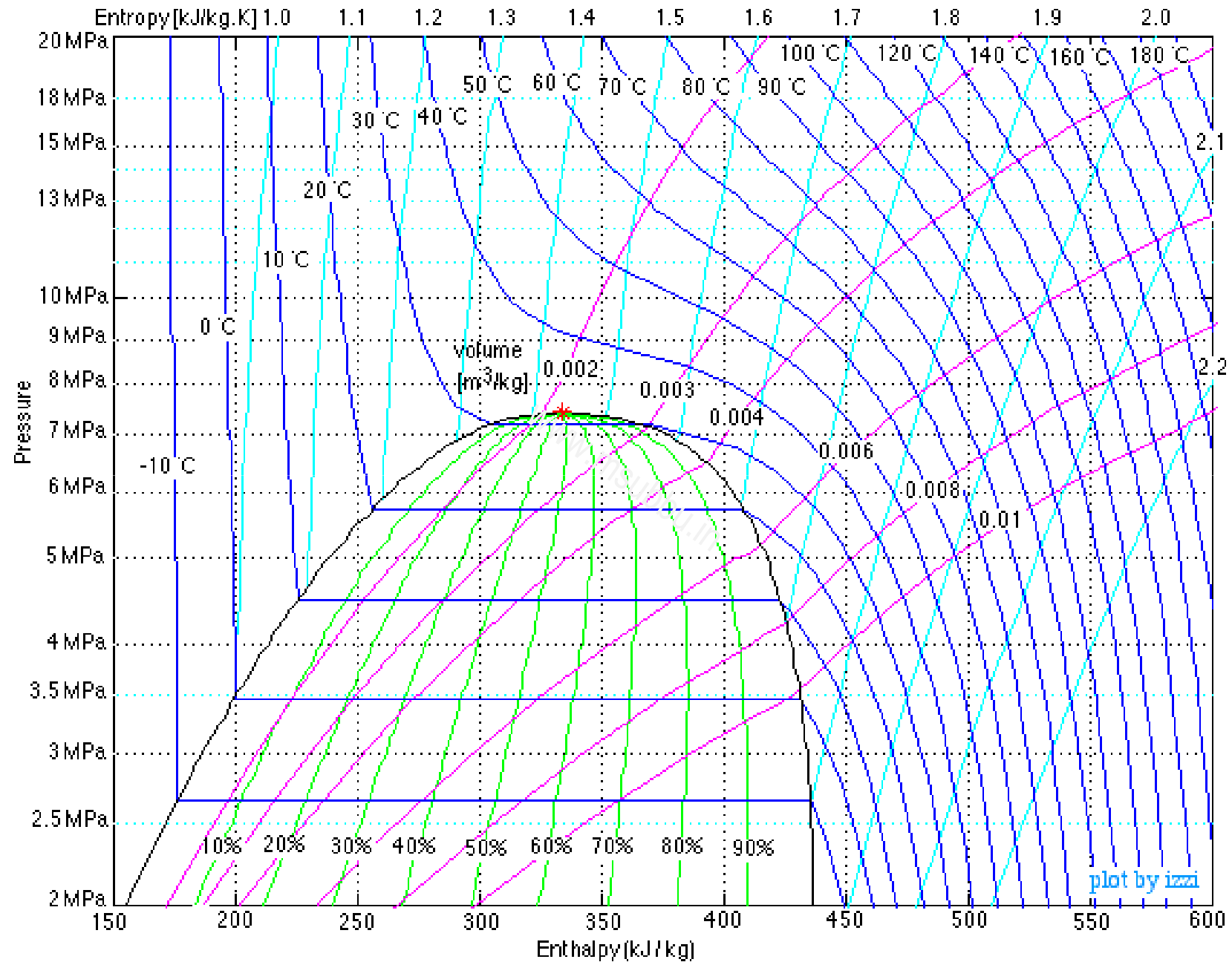
Temperature-Entropy-Diagram

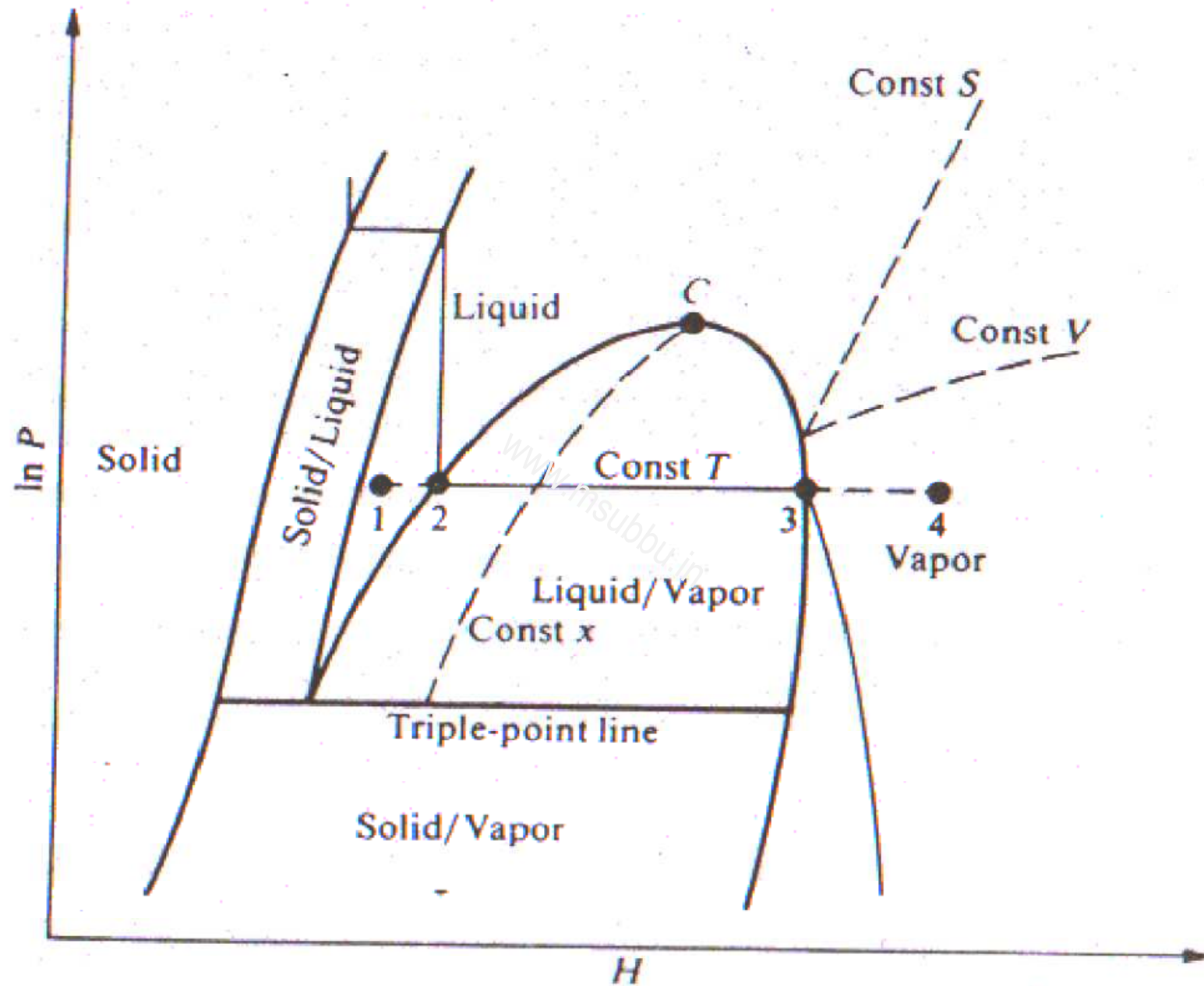




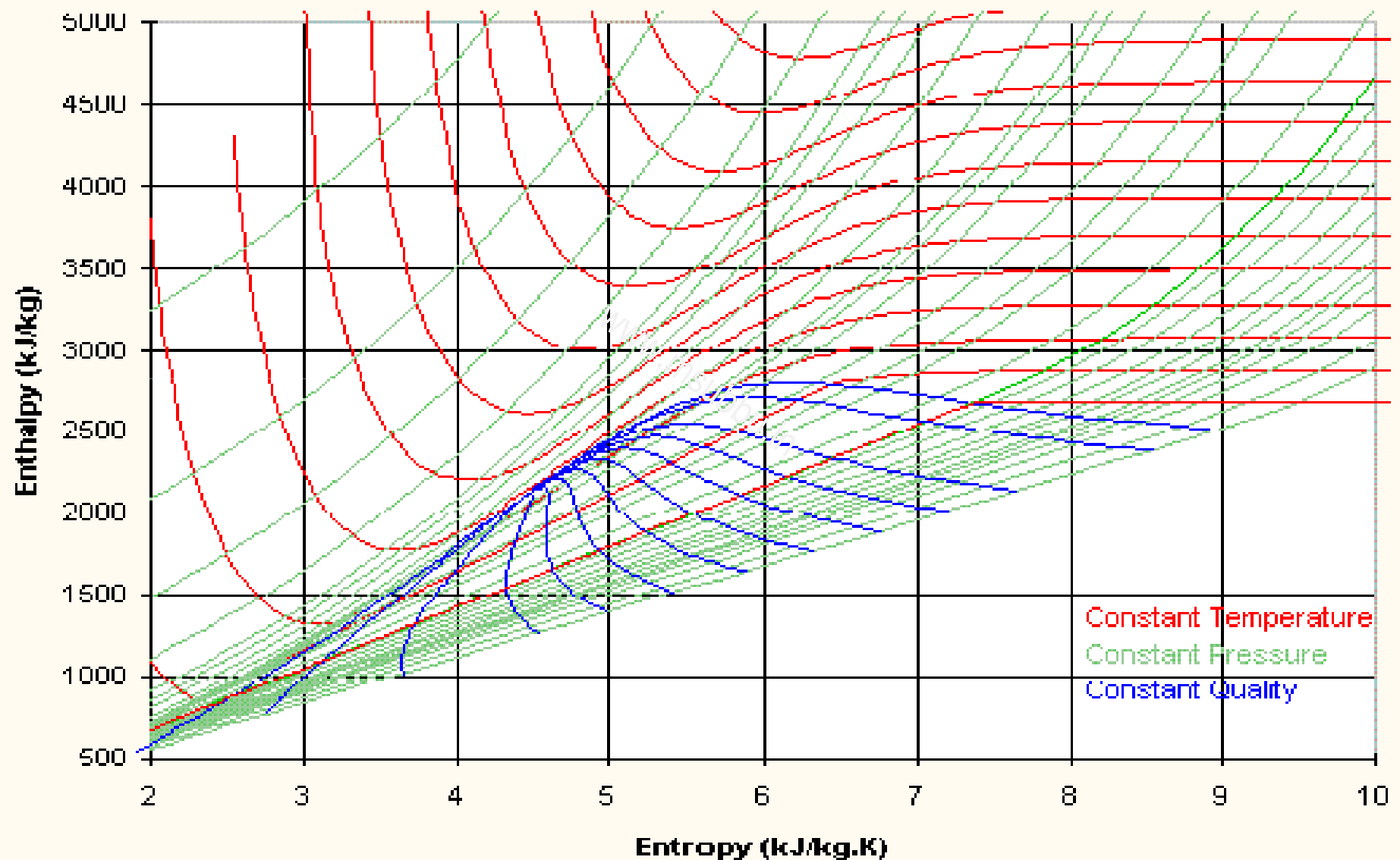


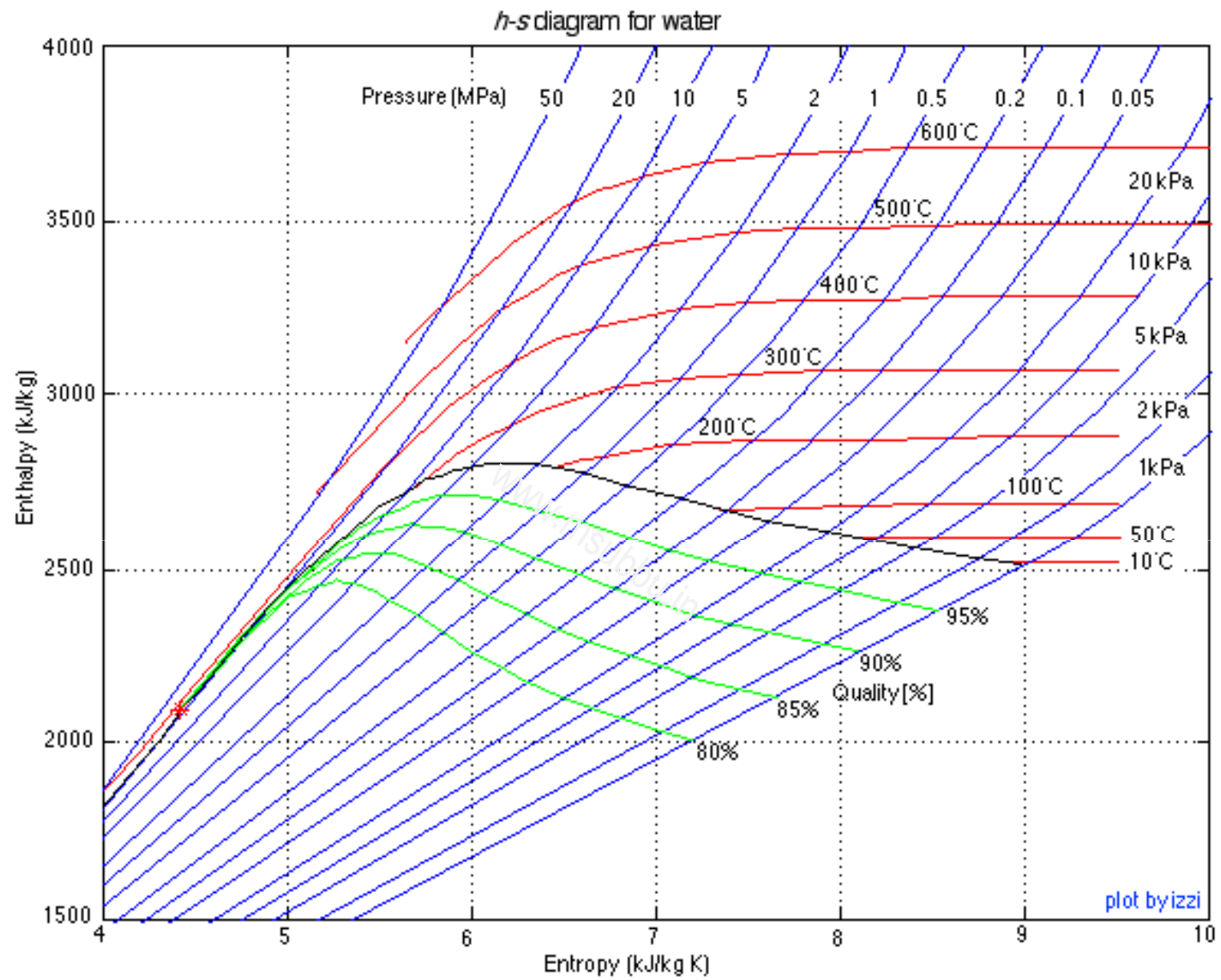
P-h diagram for Carbon Dioxide Refrigerant [R744]





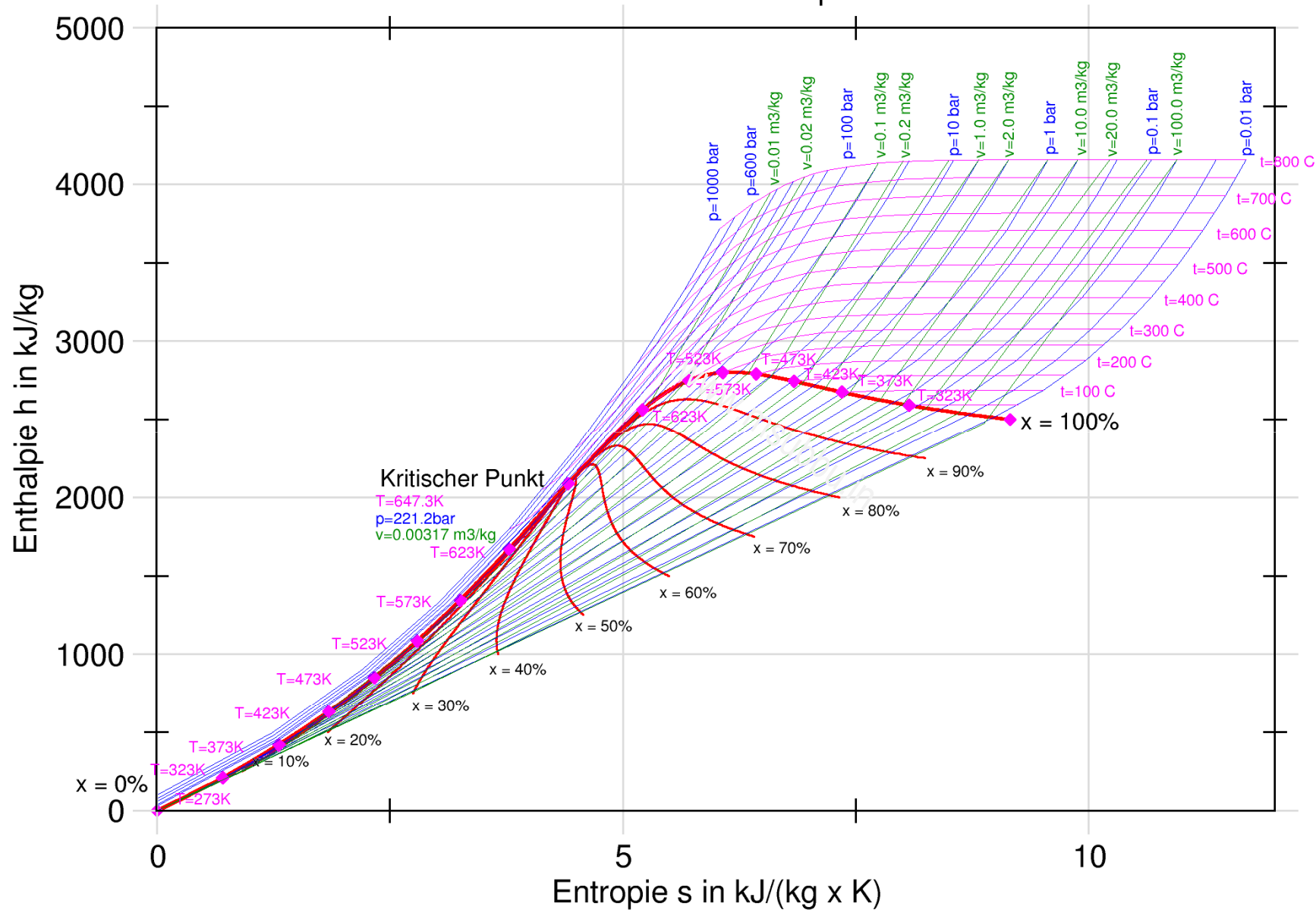
Steam97 - Moller Chart





Mollier-h, s Diagramm

fuer Wasserdampf



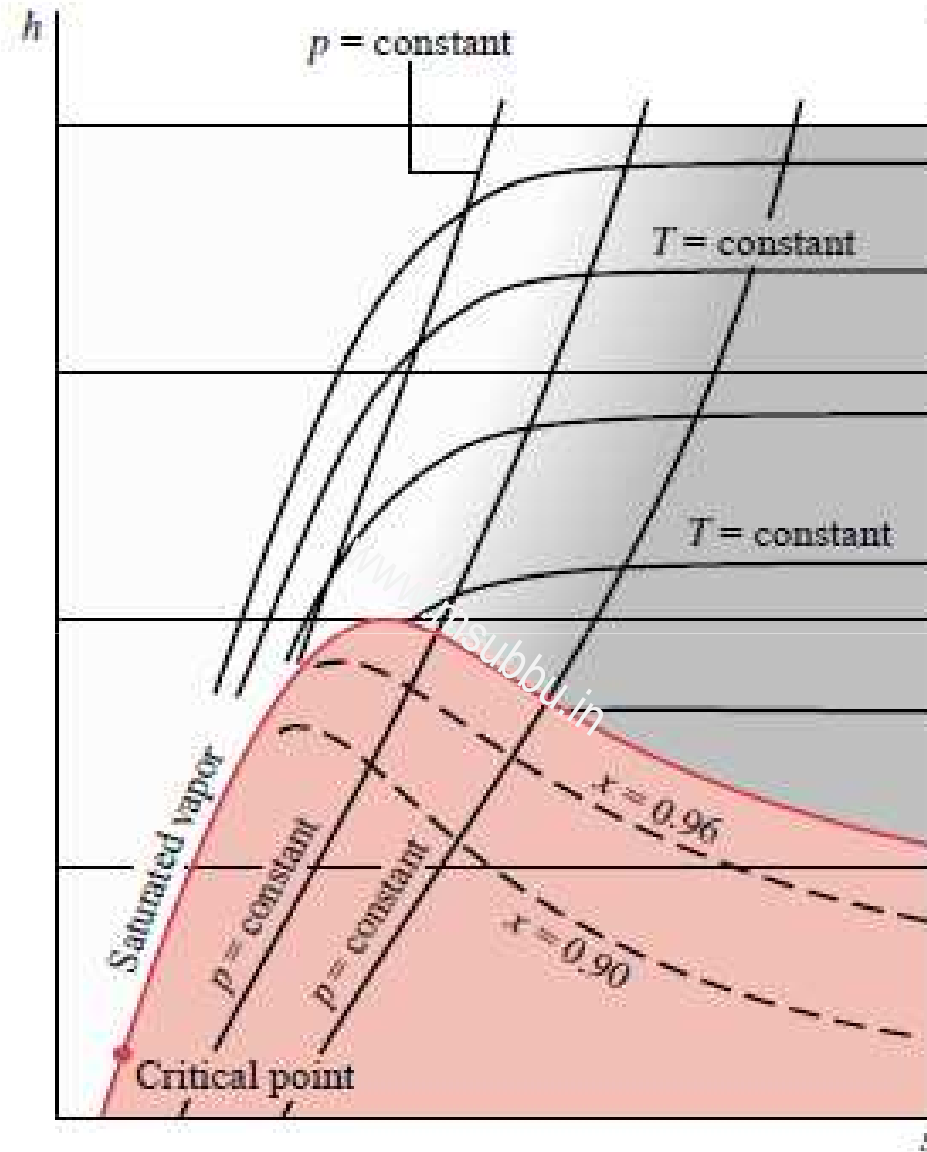


Figure 7.4 Enthalpy–entropy diagram.

Developing Thermodynamic Diagrams

TS Diagram

Experimental Data:

- (a) Vapor pressure data.
- (b) Pressure, specific volume, temperature (PVT) data in the vapor region.
- (c) Density of saturated liquid and the critical pressure and temperature.
- (d) Zero pressure specific heat data for the vapor.

1. Relation for $\ln P^{\text{sat}}$ vs. T such as

$$\ln P^{\text{sat}} = A - \frac{B}{T + C}$$

2. Equation of state for the vapor that accurately represents the PVT data.



3. State: 1

Fix values for H and S of saturated-liquid at a reference state.

4. State: 2

Enthalpy and entropy changes during vaporization are calculated from Clapeyron equation using the $\ln P^{\text{sat}}$ vs. T data as:

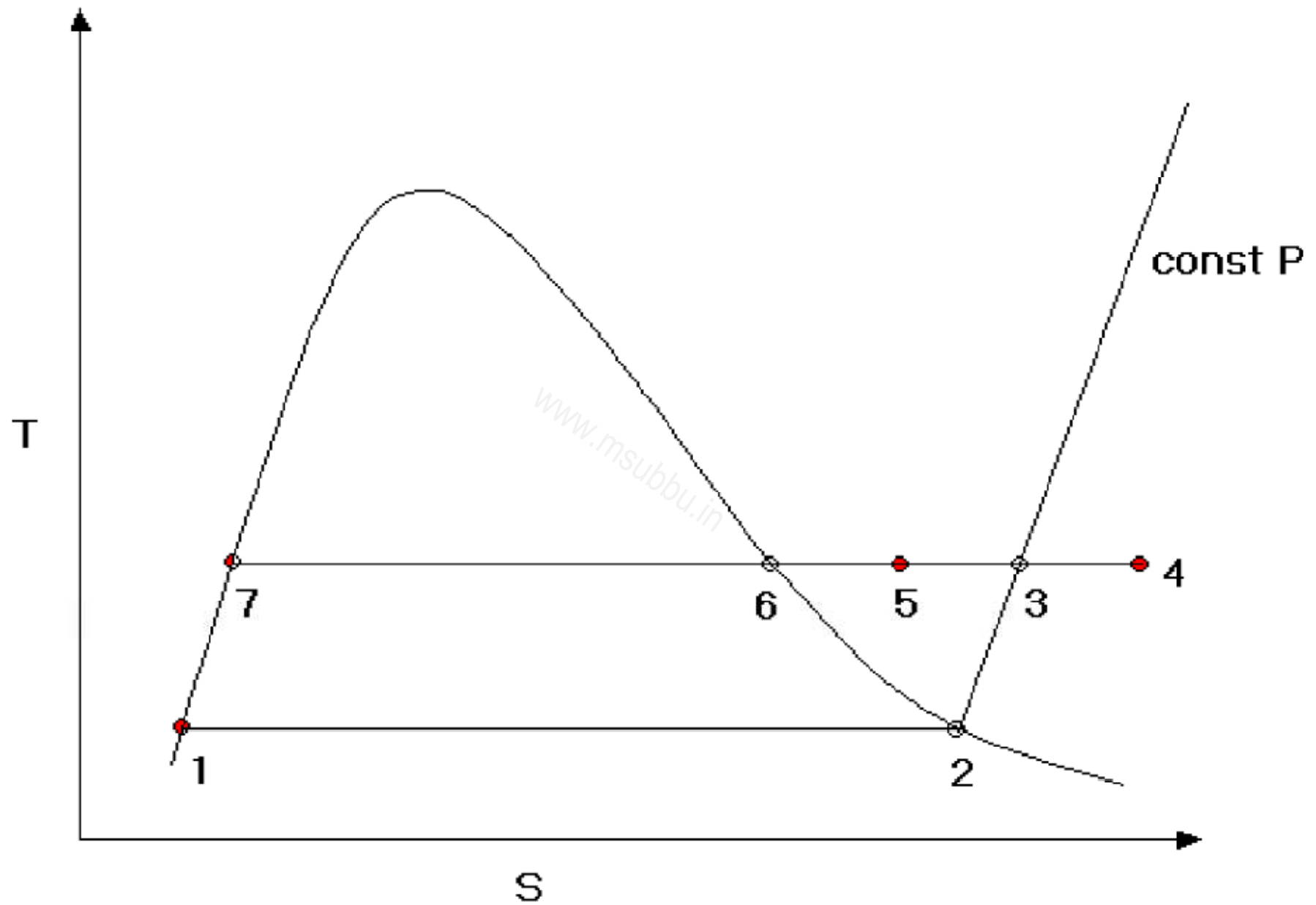
$$\frac{dP^{\text{sat}}}{dT} = \frac{\Delta H_{lv}}{T(V_v - V_l)}$$

and

$$\Delta S_{lv} = \frac{\Delta H_{lv}}{T}$$

Here V_l shall be measured, and V_v is calculated from the relation obtained in step-2.

From these values of ΔH_{vl} and ΔS_{vl} obtain the values of H and S at state: 2



5. **State: 3** Follow the constant pressure line.

$$\begin{aligned}dH &= C_P dT + \left[V - T \left(\frac{\partial V}{\partial T} \right)_P \right] dP \\dS &= C_P \frac{dT}{T} - \left(\frac{\partial V}{\partial T} \right)_P dP\end{aligned}$$

Here for the specific heat of vapor corresponding to the pressure at state: 2 is obtained from the relation:

$$\left(\frac{\partial C_P}{\partial P} \right)_T = -T \left(\frac{\partial^2 V}{\partial T^2} \right)$$

and from the zero pressure specific heat data.

With the value of C_P for this state as calculated above, S and H values at state: 3 are calculated.

6. **State: 4, 5 & 6** The above calculation can be done along constant temperature line and the values at states 4, 5 and 6 can be obtained.
7. **State: 7** The calculations made for state: 2 can be done for the temperature at state: 6.

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